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TESTING OF ROCK ANCHOR COMBINATIONS FOR VICTORIAN CLIMBING CLUB

R.I. McNamara

September 1999



Building, Construction & Engineering



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Please address all enquiries to:

The Chief CSIRO Building, Construction and Engineering P.O. Box 56 Highett Victoria 3190 AUSTRALIA

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EXECUTIVE SUMMARY

Three rock anchor combinations were tested to determine whether or not they complied with the strength requirements of British Standard BS EN 959: 1997 Mountaineering equipment - Rock anchors - Safety requirements and testing methods [1]. None of the rock anchor combinations tested passed the strength requirements of that Standard.

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TESTING OF ROCK ANCHOR COMBINATIONS FOR VICTORIAN CLIMBING CLUB

1. INTRODUCTION

1.1 General

This report was prepared by:

Structural Testing Facility
CSIRO Building, Construction and Engineering
Graham Road
Highett Victoria 3190.

For

Victorian Climbing Club C/- James McIntosh Holden Ltd Engineering MP315 241 Salmon Street Port Melbourne VIC 3207

This report was written by:

R.I. McNamara

This report was checked by:

Dr Lam Pham - Manager Structural Product and Performance Evaluation

Signed: Date: 24 Sept 99

Date test specimens received: August 1999

Date tests performed: August 1999

1.2 Aim of Testing Off A MEMOD HOMANDOR HOLD MITCHE

The aim of the testing was to determine whether or not three rock anchor combinations complied with the strength requirements of British Standard BS EN 959: 1997 Mountaineering equipment - Rock anchors - Safety requirements and testing methods [1].

2. DESCRIPTION OF ROCK ANCHOR COMBINATIONS

2.1 General

All rock anchors i.e. brackets and Ramset masonry fasteners were supplied by the Victorian Climbing Club. The $200 \times 200 \times 200$ mm strength grade N50 concrete blocks used for testing were cast and cured for 28 days by CSIRO Building Construction and Engineering. The requirement for the concrete test blocks under BS EN 959 [1], was for a compression strength of 50 ± 10 MPa. The 28 day core test results for the cured concrete blocks fell within this requirement with an average strength of 49.5 MPa. Refer concrete compression test certificate in the Appendix of this report.

2.2 Combination 1

The first test combination consisted of the fixed 2 hole - 3 mm nominal thickness bracket marked AME, fixed to the concrete block with a 10 mm diameter x 75 mm long Ramset 316 stainless steel Dynabolt in accordance with the manufacturers instructions. Note - a 10 mm diameter Dynabolt has an M8 thread. A 10 mm diameter masonry drill was used to drill an 80 mm deep hole in the concrete block. The bracket was placed over the hole in the concrete block and the Dynabolt including washer (supplied with the bracket) under nut was inserted into the bracket/concrete hole and tightened to the manufacturers recommended tightening torque of 20 Nm.

2.3 Combination 2

The second test combination consisted of the fixed 2 hole - 3 mm nominal thickness bracket marked AME, fixed to the concrete block with a 12 mm diameter x 70 mm long Ramset 316 stainless steel Dynabolt in accordance with the manufacturers instructions. Note - a 12 mm diameter Dynabolt has an M10 thread. A 12 mm diameter masonry drill was used to drill an 80 mm deep hole in the concrete block. The bracket was placed over the hole in the concrete block and the Dynabolt including washer (supplied with the bracket) under nut was inserted into the bracket/concrete hole and tightened to the manufacturers recommended tightening torque of 40 Nm.

2.4 Combination 3

The third test combination consisted of the fixed 2.5 mm nominal thickness key hole bracket marked AME, fixed to the concrete block with a 3/8 inch diameter x 3 1/2 inch long 306 stainless steel bolt using a Ramset Chemset hammer in capsule for an M10 bolt in accordance with the manufacturers instructions. A 12 mm diameter masonry drill was used to drill a 90 mm deep hole in the concrete block. The bracket was placed over the hole in the concrete block and the stainless steel bolt NOT including washer was hammered into the bracket/concrete hole to a depth that left the bearing surface of the bolt head 4 to 6 mm clear

of the concrete. The minimum curing time before testing for the Ramset Chemset adhesive was 2 hours.

3 TEST DESCRIPTION

All tests were carried out in accordance with BS EN 959 for axial and radial tests [1]. In addition to recording the maximum load and failure mode, the displacement of the rock anchor combination was monitored using machine head movement. No recommendation for the number of test specimens was given in BS EN 959 [1]. It was considered appropriate to prepare ten specimens of each rock anchor combination. Five of each rock anchor combination were tested in the axial test configuration and five in the radial test configuration.

The axial test was carried out by applying a load perpendicular to the concrete block, via the hole at the end of the bracket opposite the masonry anchor. The radial test was carried out by applying a load parallel to the concrete block, via the hole at the end of the bracket opposite the masonry anchor.

The axial and radial test configurations were as shown in BS EN 959 Figures 3 and 4 respectively.

4 RESULTS AND DISCUSSION

The results of testing are given in the table below:

Rock Anchor Combination No.	Test Direction	Specimen No.	Max. Load (kN)	Displ. at Max. Load (mm)	Acam o Failure Mode
1	axial	1/10 A	20.01	~25.00	bolt failure
(3 mm thick bracket,		2/10 A	21.59	38.41	bolt failure
10 mm dia. Dynabolt)		3/10 A	21.65	42.83	bolt failure
ed appropriate to		4/10 A	23.33	45.53	bolt failure
antique		5/10 A	21.46	39.68	bolt failure
.nodenichten kasi	radial	1/10 S	24.63	43.61	bolt failure
		2/10 S	22.22	31.84	bolt failure
ete block visure		3/10 S	26.35	36.25	bolt failure
		4/10 S	28.81	40.44	bolt failure
yd tuo bermse asv	PASS RELIDERS	5/10 S	27.64	38.54	bolt failure
2	axial	1/12 A	8.41	16.57	Thread failure / nut
(3 mm thick bracket,		2/12 A	25.12	46.58	concrete failure
12 mm dia. Dynabolt)		3/12 A	26.60	47.00	bolt failure
L bas i se	eresta ozer s	4/12 A	25.60	44.82	concrete failure
		5/12 A	22.95	37.03	bolt failure
	radial	1/12 S	26.48	28.43	bolt failure
		2/12 S	31.79	41.11	concrete failure
		3/12 S	31.95	43.02	bolt failure
		4/12 S	31.72	39.40	concrete failure
		5/12 S	28.34	~ 28.00	concrete failure
3	axial	1C A	9.99	17.74	clip failure (tension one side)
(2.5 mm thick		2C A	10.71	21.24	clip failure (tension one side)
bracket, 3/8 inch bolt		3C A	12.26	26.45	clip fail (pulled past bolt head)
Chemset into		4CA	9.90	19.01	clip failure (tension one side)
concrete)		5C A	12.47	23.45	clip fail (pulled past bolt head)
	radial	1CS	19.30	32.80	clip failure (tension one side)
		2C S	16.21	21.65	clip failure (tension one side)
		3C S	16.42	20.70	clip failure (tension one side)
		4C S	17.51	28.66	clip failure (tension one side)
		5C S	19.41	23.22	clip failure (tension one side)

The minimum load required in BS EN 959 [1] for the axial test is 15 kN. The minimum load required in BS EN 959 [1] for the radial test is 25 kN. Interpreting the Standard, it is assumed that for a rock anchor to meet the requirements of the Standard, tests must not yield results below the required minimum values for both the axial and radial tests. On this basis none of the rock anchor combinations tested pass the BS EN 959 [1] strength requirements.

If it were not for one axial test result, combination 2 using the 12 mm diameter Dynabolt may have passed the requirements. There was not apparent reason why the nut thread failed in the axial test 1/12 A.

5 CONCLUSION

None of the rock anchor combinations tested passed the strength requirements of BS EN 959 [1] as stated above in Section 4 of this report.

6 REFERENCE

British Standards Institute. Mountaineering equipment - Rock anchors - Safety requirements and test methods. British Standard BS EN 959: 1997

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APPENDIX

Concrete compression test certificate

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TDAY FOO CURED - 48.3 Mps

28 DAY FOG CURED - 66.8 Mpa

BEDAY CORES - 49.5 Mos. "*

* TEST BLOCKS WELGET OUTSIDE AND COVERED AND COVERED ATTHEOLYSING THE SHEET FOR 28 DAYS ATTEX CASTING TORRS WERE THEN TAKEN AND TESTED WELL

TO EXECUTE REQUIRED FOR TEST WAS 50.0 Mps #/- 10%

ACIYATILA



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Building, Construction and Engineering • Graham Road (PO Box 56), Highett, Victoria 3190, Australia Telephone: 61 3 9252 6000 Facsimile: 61 3 9252 6244 Web: http://www.dbce.csiro.au

CONCRETE FOR TESTING OF ROCK ANCHORS 26-08-99

ORDERED - N 50

COMPRESSIVE STRENGTH

7 DAY FOG CURED - 48.3 Mpa

28 DAY FOG CURED - 66.8 Mpa

28 DAY CORES - 49.5 Mpa **

** TEST BLOCKS WERE CAST OUTSIDE AND COVERED WITH POLYETHELENE SHEET FOR 28 DAYS AFTER CASTING. CORES WERE THEN TAKEN AND TESTED WET.

STRENGTH REQUIRED FOR TEST WAS 50.0 Mpa +/- 10%

A.H.TAYLOR

SENIOR TECHNICAL OFFICER