

# Hydrodynamic Interactions Introduce Differences in the Behaviour of a Ratchet Dimer Brownian Motor

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## Abstract

We use the Brownian dynamics with hydrodynamic interactions simulation in order to describe the movement of an elastically coupled dimer Brownian motor in a ratchet potential. The only external forces considered in our system were the load, the random thermal noise and an unbiased thermal fluctuation. We observe differences in the dynamic behaviour if hydrodynamic interactions are considered as compared with the case without them. In conclusion, hydrodynamic interactions influence substantially the dynamics of a ratchet dimer Brownian motor; consequently they have to be considered in any theory where the molecular motors are in a liquid medium.

## Keywords

Hydrodynamic Interactions, Motor Proteins, Molecular Dynamics, Brownian Dynamics, Fluctuation Phenomena, Random Processes, Noise, Brownian Motion

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## 1. Introduction

Brownian motors are small physical micro- or even nano-machines that operate far from thermal equilibrium by extracting the energy from both thermal and non-equilibrium fluctuations in order to generate work against external loads. They present the physical analogue of bio-molecular motors that also work out of equilibrium to direct intracellular transport and to control motion in cells. In such bio-molecular motors, proteins such as kinesins, myosins and dyneins, move unidirectionally on one-dimensional “tracks” while hydrolysing adenosine triphosphate (ATP). These molecular motors are powered by a ratchet mechanism [1]; they convert the nonequilibrium fluctuation into directed flow of Brownian particles in an asymmetrical periodic potential (ratchet) with-

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out any net external force or bias. Several authors have studied theoretically the transport of two coupled particles modeling the two heads of a motor protein [2]-[13]. Nonequilibrium fluctuations, whether generated or by a chemical reaction far from equilibrium, can bias the Brownian motion of a particle in an anisotropic medium without thermal gradients, a net force such as gravity, or a macroscopic electric field. Fluctuation-driven transport is one mechanism by which chemical energy can directly drive the motion of particles and macromolecules and may find application in a wide variety of fields, including particle separation and the design of molecular motors and pumps. Zimmermann and Seifert [14] studied the efficiencies of a molecular motor for a generic hybrid model applied to the F1-ATPase, and they obtained good quantitative agreement with the experimental data. Pinkoviezky and Gov [15] were motivated by the observed pulses of backward-moving myosin-X in the filopodia structure, and they modelled interacting molecular motors with an internal degree of freedom, introducing a novel modification to the approximation scheme.

In the present work, we use the Brownian dynamics with hydrodynamic interactions simulation in order to describe the movement of an elastically coupled dimer Brownian motor in a ratchet potential. In Section 2, we describe the forces acting on an oscillating dimer in a ratchet potential with a load force and an external unbiased fluctuation, which acts simultaneously on two particles. In Section 3, we describe the formalism given by Ermak and McCammon (1978) [16], which couples the forces described in Section 2 and thermal noise with the diffusion tensor. A striking feature of fluid mechanics in the viscously dominated regime, or equivalently, at low Reynolds number, is the long range of hydrodynamic interactions. For example, the Stokeslet, or flow field induced by a point force, falls off inversely with distance. Hydrodynamic interactions have been considered by several authors to explain different phenomena. Kems and Bhattacharjee, [17], used a particle tracking model for colloid transport near planar surfaces covered with spherical asperities. This model provides a preliminary step in investigating how geometrically tractable asperities alter the undisturbed flow field and hydrodynamic interactions between the particle and the substrate. Hydrodynamic interactions allow in average for directed motion of a three-sphere system, and the spheres are connected by two identical active linker arms. Each linker arm contains molecular motors and elastic elements and can oscillate spontaneously; see [18]. Microorganisms are often subjected to swimming in close proximity to each other as well as other boundaries. The resulting hydrodynamic interactions may have puzzling effects on their swimming speed, trajectory, and power dissipation. These effects were investigated by Ramia *et al.* [19]; each microorganism consisted of a sphere propelled by a rotating helix. It was found that only a small increase (less than 10%) resulted in the mean swimming speed of an organism swimming near and parallel to another identical organism. In a later paper, [20] focused on hydrodynamic interactions by considering two rotating rigid helices. They supposed that the helices were driven by stationary motors, and obtained complementary results to those of Ramia *et al.*, since the hydrodynamic interactions between their helices were stronger. Recently Fornés, [21], showed that hydrodynamic interactions induced movement against an external load in a ratchet dimer Brownian motor. In the present paper, we show that hydrodynamic interactions introduce differences in the behaviour of a ratchet dimer Brownian motor as compared without them. We report differences in the Peclet number, effective diffusion coefficient, mean  $x$  component of the mass center position and velocity and particles positions cross correlations in  $x$  direction.

## 2. The Model

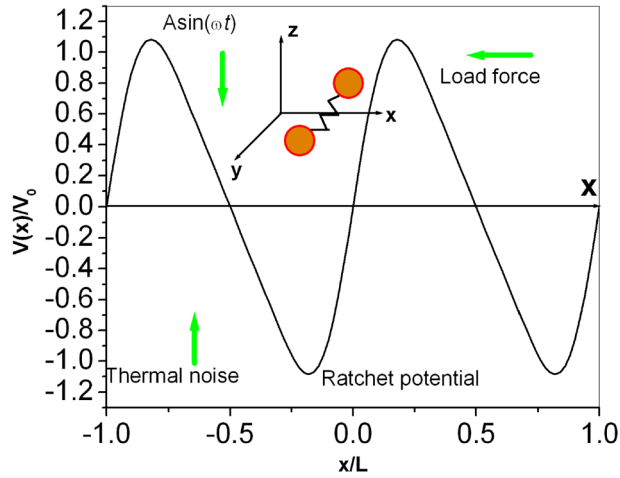
We consider an elastically coupled dimer in 3 dimensions in an asymmetrical potential (ratchet) in the  $x$  direction, see **Figure 1**. We considered a linear superposition of three spatial harmonics, following Ref. [22],

$$U_{\text{rat}}(x_i) = V_0 \left[ \sin\left(\frac{2\pi x_i}{L}\right) + c_1 \sin\left(\frac{4\pi x_i}{L}\right) + c_2 \sin\left(\frac{6\pi x_i}{L}\right) \right]. \quad (1)$$

The corresponding force on the particles produced by the ratchet potential is given by:

$$F_{\text{rat}}(x_i) = -\frac{\partial U_{\text{rat}}(x_i)}{\partial x_i} = -\frac{2\pi V_0}{L} \left[ \cos\left(\frac{2\pi x_i}{L}\right) + 2c_1 \cos\left(\frac{4\pi x_i}{L}\right) + 3c_2 \cos\left(\frac{6\pi x_i}{L}\right) \right]. \quad (2)$$

In the former equations  $x_i$  is the  $x$  coordinate of particle  $i$ ,  $i=1$  and  $2$ , to distinguish the dimer particles. The parameters  $c_1$  and  $c_2$  determine the ratchet profile. We use the parameters from Ref. [22]:  $c_1 = 0.245$ ,  $c_2 = 0.04$  and  $V_0 = 0.461$ .



**Figure 1.** Dimer in an asymmetrical ratchet potential under a constant load force, thermal noise and unbiased thermal sinusoidal fluctuation.

We define  $\mathbf{r}_{ij}$  the vector from the center of particle  $i$  to the center of particle  $j$ , for particles  $i = 1, j = 2$ , we have

$$\mathbf{r}_{ij} = x_{12}\mathbf{i} + y_{12}\mathbf{j} + z_{12}\mathbf{k} \quad (3)$$

$\mathbf{i}, \mathbf{j}, \mathbf{k}$  are unit vectors in the direction of the cartesian axis, with

$$\begin{aligned} x_{12} &= x_1 - x_2; \\ y_{12} &= y_1 - y_2; \\ z_{12} &= z_1 - z_2; \\ r_{12} &= (x_{12}^2 + y_{12}^2 + z_{12}^2)^{1/2}. \end{aligned} \quad (4)$$

Then the modulus of the harmonic force is,

$$F_{12} = |k(l_0 - r_{12})| \quad (5)$$

where  $k$  is the strength of the harmonic potential and  $l_0$  is the equilibrium position.

Then the components of the harmonic force are,

$$\begin{aligned} F_{x_{12}} &= F_{12} \frac{x_{12}}{r_{12}}; \\ F_{y_{12}} &= F_{12} \frac{y_{12}}{r_{12}}; \\ F_{z_{12}} &= F_{12} \frac{z_{12}}{r_{12}}. \end{aligned} \quad (6)$$

The corresponding components of the harmonic force on each dimer particle are,

$$\begin{aligned} F_{\text{har}}(x_1) &= F_{12} \frac{x_{12}}{r_{12}} = -F_{\text{har}}(x_2); \\ F_{\text{har}}(y_1) &= F_{12} \frac{y_{12}}{r_{12}} = -F_{\text{har}}(y_2); \\ F_{\text{har}}(z_1) &= F_{12} \frac{z_{12}}{r_{12}} = -F_{\text{har}}(z_2). \end{aligned} \quad (7)$$

Then the forces acting on the dimer particles are:

$$\begin{aligned}
 F_{x1} &= F_{\text{har}}(x_1) + F_{\text{rat}}(x_1) - F_{\text{load}} + \varepsilon_x(t); \\
 F_{y1} &= F_{\text{har}}(y_1); \\
 F_{z1} &= F_{\text{har}}(z_1); \\
 F_{x2} &= -F_{\text{har}}(x_1) + F_{\text{rat}}(x_2) - F_{\text{load}} + \varepsilon_x(t); \\
 F_{y2} &= -F_{\text{har}}(y_1); \\
 F_{z2} &= -F_{\text{har}}(z_1).
 \end{aligned} \tag{8}$$

The load force,  $F_{\text{load}}$ , acts to oppose the motors forward progress,  $\varepsilon_x(t) = A \sin(\omega t)$  is an external unbiased fluctuation, which acts simultaneously on two particles.

### 3. Brownian Dynamics with Hydrodynamic Interactions

Consider a system of  $N$  spherical interacting Brownian particles suspended in a hydrodynamic medium, the displacement of particle  $i$  during  $\Delta t$  is given by Ermak and McCammon (1978) [16], namely

$$r_i = r_i^0 + \sum_j \frac{D_{ij}^0 F_j^0}{k_B T} \Delta t + R_i(\Delta t) \tag{9}$$

where the superscript ‘‘0’’ indicates that the variable is to be evaluated at the beginning of the time step.  $F_j^0$  is the force acting on particle  $j$ .  $R_i(\Delta t)$  is a random displacement with a Gaussian distribution function whose average value is zero and the correlation is  $\langle R_i(\Delta t) R_j(\Delta t) \rangle = 2D_{ij}^0 \Delta t$ .

$$\begin{aligned}
 D_{ij}^0 &= D_0 \delta_{ij}, \quad i, j \text{ on the same particle,} \\
 D_{ij}^0 &= \frac{3}{4} D_0 \frac{a}{r_{ij}} \left( I + \frac{\overline{r_{ij}} \otimes \overline{r_{ij}}}{r_{ij}^2} \right), \quad i, j \text{ on different particles.}
 \end{aligned} \tag{10}$$

$D_0 = kT/6\pi\eta a$  is the diffusion coefficient of a single subunit sphere of  $a$  radius,  $\overline{r_{ij}} \otimes \overline{r_{ij}}$  is the dyadic product, for particles  $i = 1, j = 2$ , we have

$$\overline{r_{12}} \otimes \overline{r_{12}} = \begin{bmatrix} x_{12} \\ y_{12} \\ z_{12} \end{bmatrix} \begin{bmatrix} x_{12} & y_{12} & z_{12} \end{bmatrix} = \begin{bmatrix} x_{12}^2 & x_{12}y_{12} & x_{12}z_{12} \\ y_{12}x_{12} & y_{12}^2 & y_{12}z_{12} \\ z_{12}x_{12} & z_{12}y_{12} & z_{12}^2 \end{bmatrix}. \tag{11}$$

In our case of a dimer in three dimensions the tensor  $D_{ij}^0$  is a  $6 \times 6$  matrix. For details on hydrodynamic interactions see our recent article [21] [23] [24], also Refs. [25] [26].

A first basic quantity of interest, in our case, is the average center of mass velocity in the  $x$  direction,  $\langle v_{cx} \rangle$ , in the long-time limit, *i.e.*, after transients due to initial conditions have died out, is given by

$$\langle v_{cx} \rangle = \left\langle \dot{r}_{cx}(t) \right\rangle_{st} = \lim_{t \rightarrow \infty} \frac{\langle x_c(t) \rangle - \langle x_c(0) \rangle}{t} \tag{12}$$

where  $r_{cx}(t) = [x_1(t) + x_2(t)]/2$ .

Another quantity of central interest will be the effective diffusion coefficient,

$$D_{\text{eff}} = \lim_{t \rightarrow \infty} \frac{\langle r_c(t)^2 \rangle - \langle r_c(0) \rangle^2}{2t} = \lim_{t \rightarrow \infty} \frac{\sigma_{r_c}^2}{2t} \tag{13}$$

where  $r_c = (r_{cx}^2 + r_{cy}^2 + r_{cz}^2)^{1/2}$ . The means are over the realizations of the stochastic process.

The competition between the drift  $v$  and diffusivity  $D_{\text{eff}}$  in advection-diffusion problems is often expressed by a dimensionless number, the Péclet number,  $Pe$ , [27],

$$Pe = \frac{|v|L}{D_{\text{eff}}} \tag{14}$$

here  $L$  is a typical length scale, in our case the length of a single ratchet element,  $v$  is the average stationary velocity of the particle, in our case we used  $|\langle v_{cx} \rangle|$ . The larger the Péclet number, the more net drift predominates over diffusion.

### 4. Results

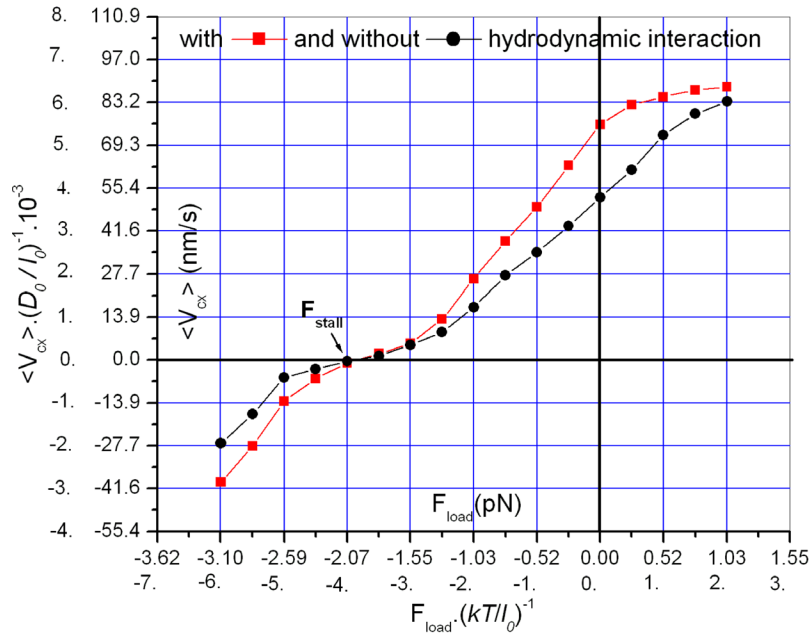
We performed the simulation in dimensionless units. Distance is in units of the separation distance  $l_0$  and time is in units of  $l_0^2/D_0$ . We used in the simulations the following parameters:  $l_0 = 1$ ,  $L = 1$ ,  $k = 100$ ,  $a = 0.281$ ,  $D_0 = 10^{-3}$ ,  $A = 3.7$ ,  $\omega = 4.9$ ,  $\Delta t = 0.00125$ , the simulation time was  $t = 1125$ , which corresponds to  $9 \times 10^5$  steps. The corresponding dimension units are:  $l_0 = 8 \text{ nm}$ ,  $L = 8 \text{ nm}$ ,  $k = 6.47 \text{ pN/nm}$ ,  $a = 2.5 \text{ \AA}$ ,  $D_0 = 10^{-3} \times kT/6\pi\eta a = 1.109 \times 10^{-13} \text{ m}^2/\text{s}$ ,  $A = 1.91 \text{ pN}$ ,  $\omega = 8.491 \text{ kHz}$ ,  $\Delta t = 0.721 \text{ \mu s}$ . In Brownian dynamics simulations with hydrodynamic interactions the size of the physically meaningful time step is restricted to values which are sufficiently long  $\Delta t \gg m_i D_0/kT$ . In our case  $m_i D_0/kT = 3.4 \text{ fs}$  where we have used  $m_i = 138 \times 10^{-24} \text{ Kg}$  for the protein dimer unit of  $2.5 \text{ \AA}$  of radius.

The average velocity of a molecular motor is a function of the load force resisting the motor's advancement. One of the characteristic of a molecular motor is the load force-velocity curve. In **Figure 2** we show  $\langle v_{cx} \rangle$  as a function of the load force  $F_{\text{load}}$ . Each point of the curve of **Figure 2** is the result of 500 stochastic realizations. At the stationary state, the ratio  $SE(\langle v_{cx} \rangle)/\langle v_{cx} \rangle \leq 10^{-6}$ , where  $SE(\langle v_{cx} \rangle)$  is the standard error of the mean velocity  $\langle v_{cx} \rangle$ .

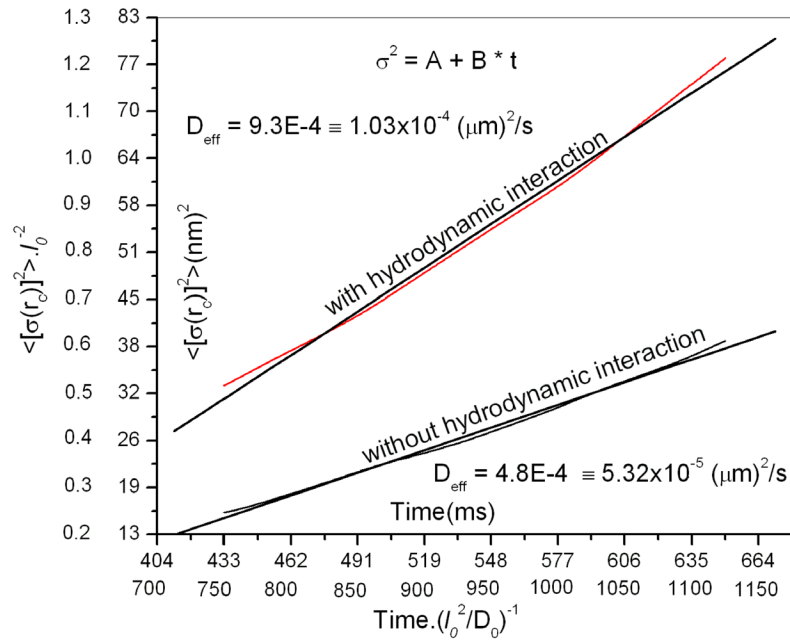
In the range  $-4 \leq F_{\text{load}} \leq 0$  we observe, the motor continue with a positive velocity in spite of the negative load force (motor effect). We also observe a substantially increase of the motor velocity in the case with hydrodynamic interaction as compared without it.

In **Figure 3**, we observe the behaviour of the mass center position variance,  $\sigma^2(r_c(t)) = \langle (r_c(t))^2 \rangle - \langle r_c(t) \rangle^2$ , as a function of time in the long time limit, *i.e.*, after transients due to initial conditions have died out. The effective diffusion coefficient is giving by the slope of the linear fitting,  $D_{\text{eff}} = 0.5B$  in accordance to Equation (13), we observe greater slope for the case with hydrodynamic interactions.

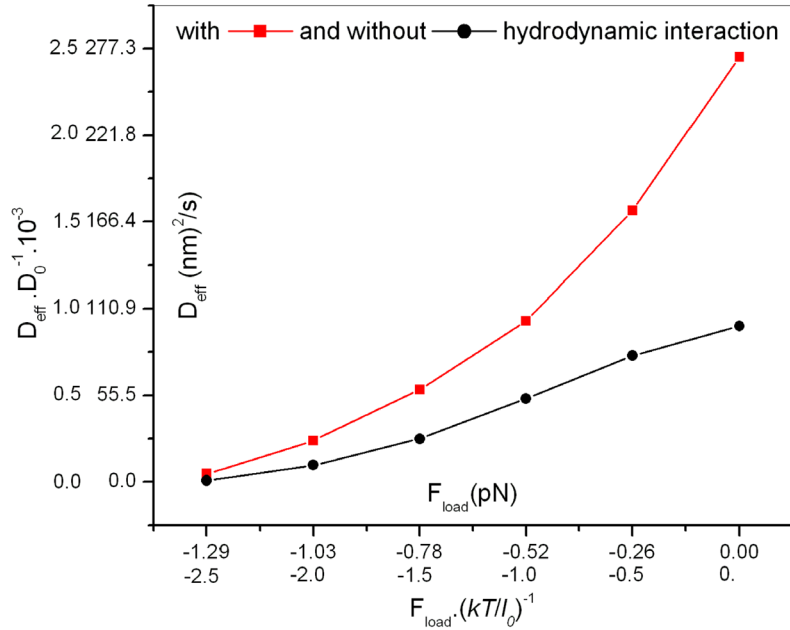
In **Figure 4** is shown the effective diffusion coefficient as a function of the load force,  $D_{\text{eff}}$  vs  $F_{\text{load}}$ , we observe that hydrodynamic interactions increase the effective diffusion.



**Figure 2.** Mean  $x$  component of the mass center velocity versus the load force,  $\langle v_{cx} \rangle$  vs  $F_{\text{load}}$ .



**Figure 3.** Variance of the mass center position,  $\sigma^2(r_c(t)) = \langle (r_c(t))^2 \rangle - \langle r_c(t) \rangle^2$ , as a function of time in the long time limit. The effective diffusion coefficient is giving by the slope of the linear fitting,  $D_{\text{eff}} = 0.5B$ , in accordance to Equation (13).  $F_{\text{load}} = -1$ .



**Figure 4.** The effective diffusion coefficient as a function of the load force,  $D_{\text{eff}}$  vs  $F_{\text{load}}$ .

In **Figure 5** is shown the Péclet number as a function of the load force,  $Pe$  vs  $F_{\text{load}}$ , we observe lower Péclet numbers for the case with hydrodynamic interactions, meaning that the net drift diminish over diffusion as compared with the case without hydrodynamic interactions.

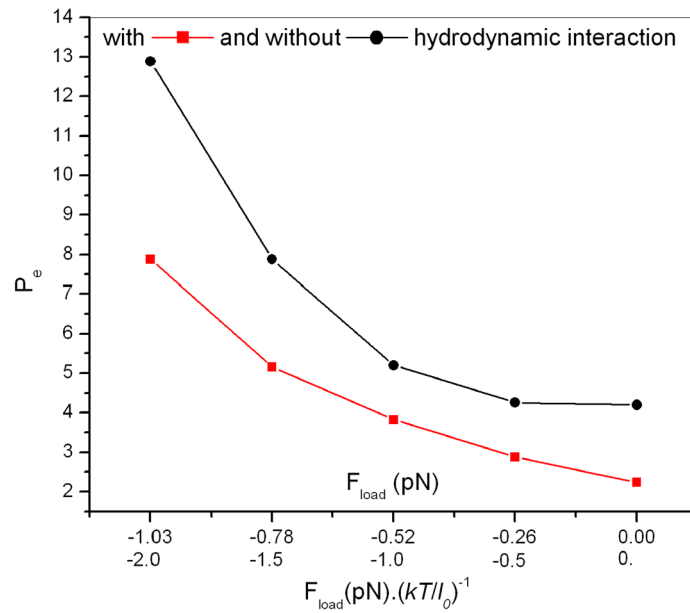


Figure 5. Péclet number as a function of the load force,  $Pe$  versus  $F_{load}$ .

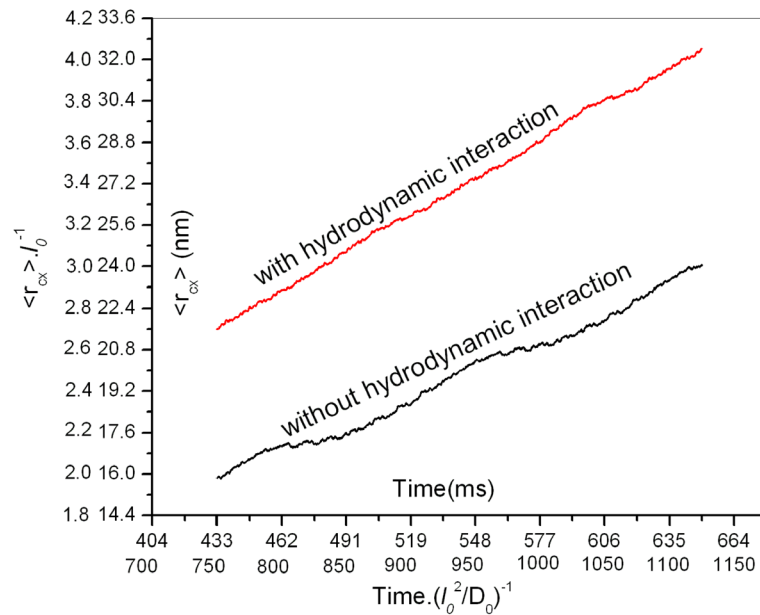
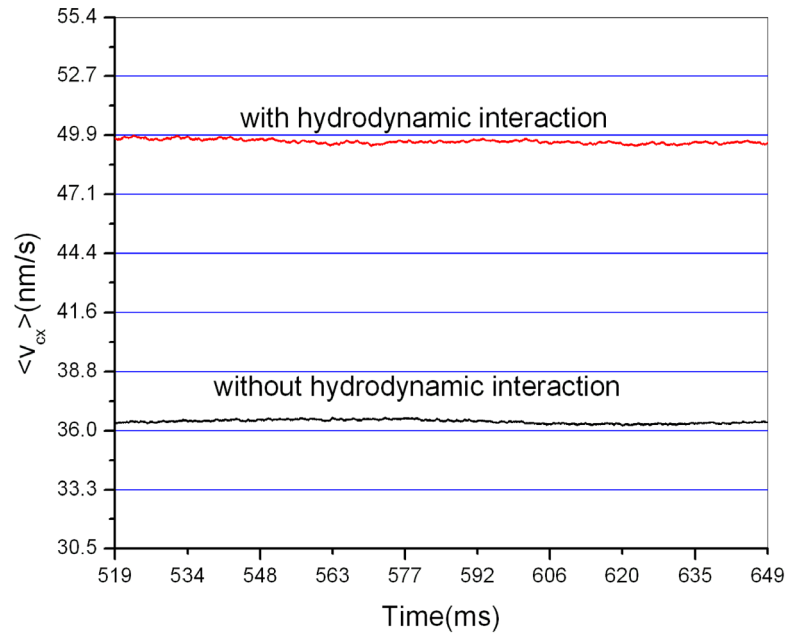


Figure 6. Mean  $x$  component of the mass center position as a function of time,  $\langle r_{cx} \rangle$  versus time. In the long time limit.  $F_{load} = -1$ .

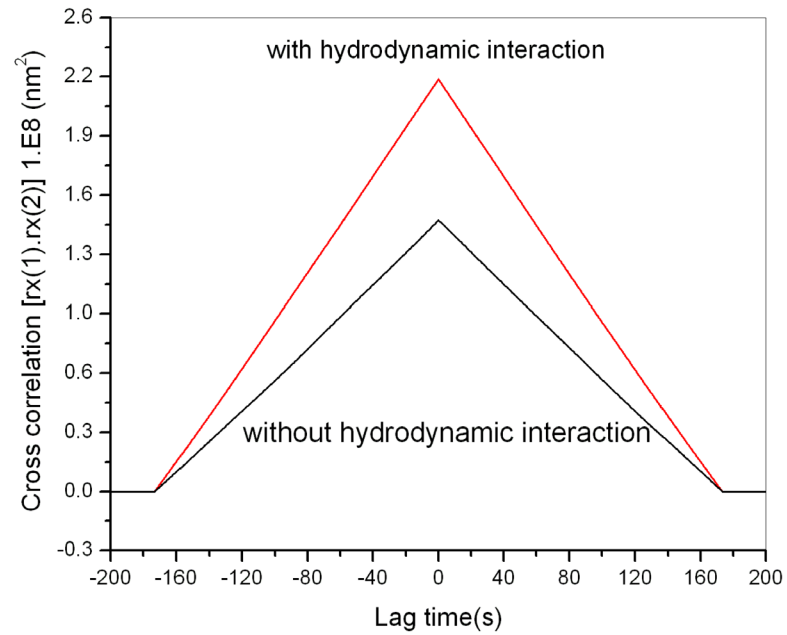
In Figure 6 is shown the mean  $x$  component of the mass center position as a function of time,  $\langle r_{cx} \rangle$  versus time, in the long-time limit, for a given load force,  $F_{load} = -1$ . We observe a linear relation, with  $\langle r_{cx} \rangle$  in the case with hydrodynamic interactions greater than the case without them.

In Figure 7 we observe the behaviour of the average center of mass velocity in the  $x$  direction,  $\langle v_{cx} \rangle$  versus time, in the long-time limit for a given load force,  $F_{load} = -1$ . The velocity is substantially greater for the case with hydrodynamic interactions.

In Figure 8 is shown the spatial cross correlations in  $x$  direction as a function of Lag time,  $\text{Corr}[r_x(1), r_x(2)]$  versus Lag time. We observe that the correlation is higher in the case with hydrodynamic interactions.



**Figure 7.** Mean  $x$  component of the mass center velocity as a function of time,  $\langle v_{cx} \rangle$  versus time. In the long time limit.  $F_{\text{load}} = -1$ .



**Figure 8.** Spatial cross correlations in  $x$  direction as a function of lag time,  $\text{Corr}[r_x(1), r_x(2)]$  versus Lag time.  $\text{Corr}[r_x(1), r_x(2)]_j = \sum_{k=0}^{N-1} r_x(1)_{j+k} r_x(2)_k$   $F_{\text{load}} = -1$ .

A similar result was found by Houtman *et al.* [28] who developed a simple 2D-lattice model in order to test the influence of hydrodynamic interactions on the collective transport of molecular motors, which is important for the understanding of cell growth and development. Houtman *et al.* showed that long range collective hydrodynamic interactions lead to a substantial increase in the effective velocity of motors attached to a filament. Their results were also supported by experiments.



## 5. Conclusion

In conclusion, hydrodynamic interactions influence substantially the dynamics of a ratchet dimer Brownian motor; consequently they have to be considered in any theory where the molecular motors are in a liquid medium.

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